

High Heat Flux Testing of PFCs for SPARC

3rd Annual INFUSE Workshop

Dec 16th, 2021

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High Heat Flux (HHF) Programmatic Goals

- SPARC is a short-pulse (10 s), high power density tokamak to demonstrate net fusion energy
- baseline divertor operation is to sweep the strike point over inertially cooled divertor ($>100 \text{ MW/m}^2$ divertor surface heat flux)
- INFUSE project aims to
 1. Inform the divertor plasma-facing material choice 
 2. Demonstrate that the plasma-facing component can survive under SPARC-relevant cyclic heat loading 

INFUSE collaborators have been flexible to adapt to the evolving needs to apply these aims to an in-progress PFC design activity

- design activities have led to concepts where low/high cycle fatigue at the component level is no longer a specific concern that requires HHF testing
- Improved output of program at the plasma facing material choice level

INFUSE Activity Has Adapted to SPARC Needs



- SPARC material down-selection in January 2021 chose tungsten-based materials over carbon-based, identified potential of tungsten heavy alloys
 - INFUSE testing helped to inform damage limits & failure modes which led to inclusion of this alloy in SPARC baseline PFC design
- SPARC value engineering emphasizing ‘design to manufacture’, led to outreach to tungsten suppliers/fabricators
 - upcoming tests to cross-compare surface cutting techniques, speed vs. heat flux handling performance & surface damage

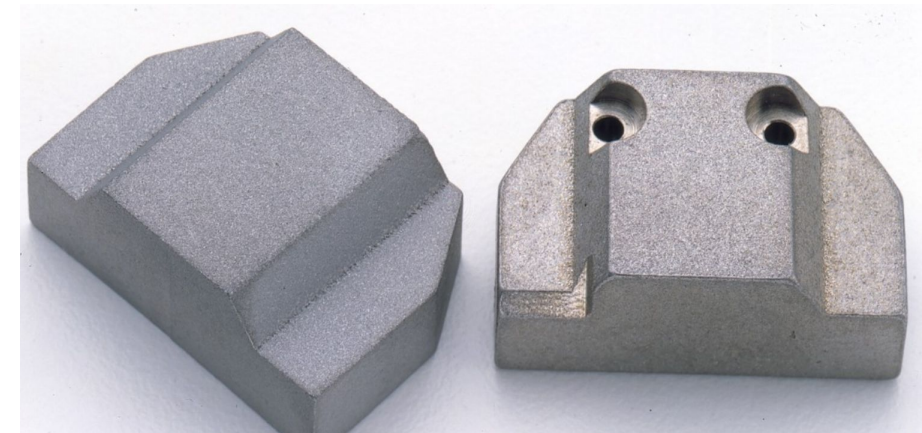
Tasks	2020				2021				2022
	Q1	Q2	Q3	Q4	Q1	Q2	Q3	Q4	Q1
Test calibration w/ pure-W									
Pure-W vs. WHA comparisons									
Pure-W fabrication comparisons									

Why is the SPARC PFC Design Using WHA?

- favorable tests in ASDEX Upgrade divertor tiles [Neu JNM 2018]
- WHA thermal properties result in similar rise in temperature for steady-state, pulsed heat flux (up to $T_{\text{limit, WHA}}$), despite $k(T)$ being different than pure-W
 - downside is the reduced temperature limit due to the presence of Ni and Fe, limiting bulk temperatures to the melt temperature ~ 1500 degC
- WHA behaves like a ductile material at all temperatures, not just $T_w > \text{DBBT}$
- WHA has a RT resistivity of $\sim 11 \mu\Omega\text{-cm}$ vs. $\sim 5 \mu\Omega\text{-cm}$ for pure-W which translates directly to eddy current load reduction

WHA has lower risk for 'cold disruptions' when using thick, inertially cooled PFM in high-field devices

- at large QTY, WHA fabricated from near-net-shape pressing + final machining, opening up wider tile shapes at similar cost, duration points

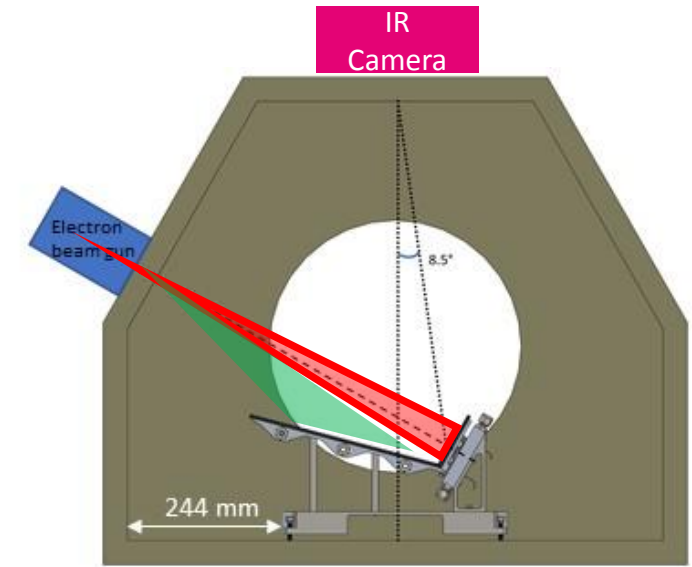


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W/WHA Tests to Failure at SPARC Heat Fluxes



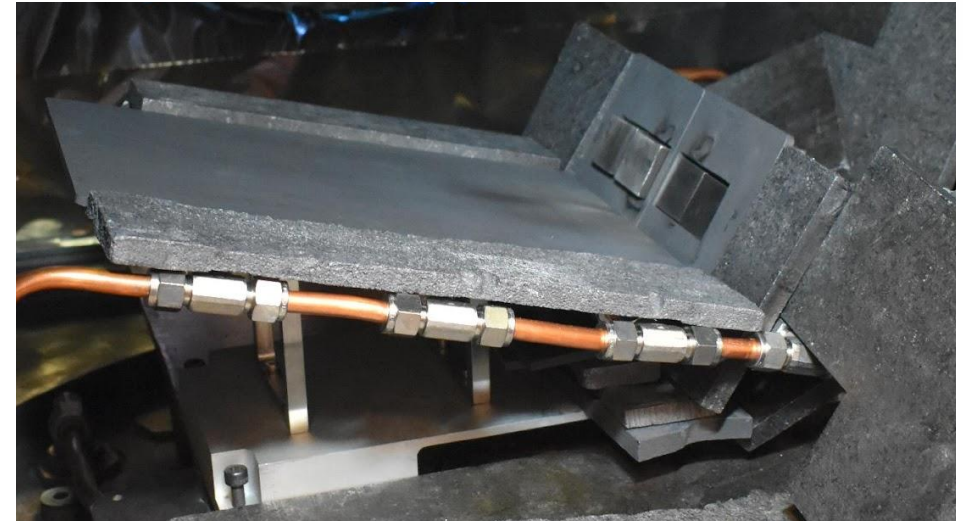
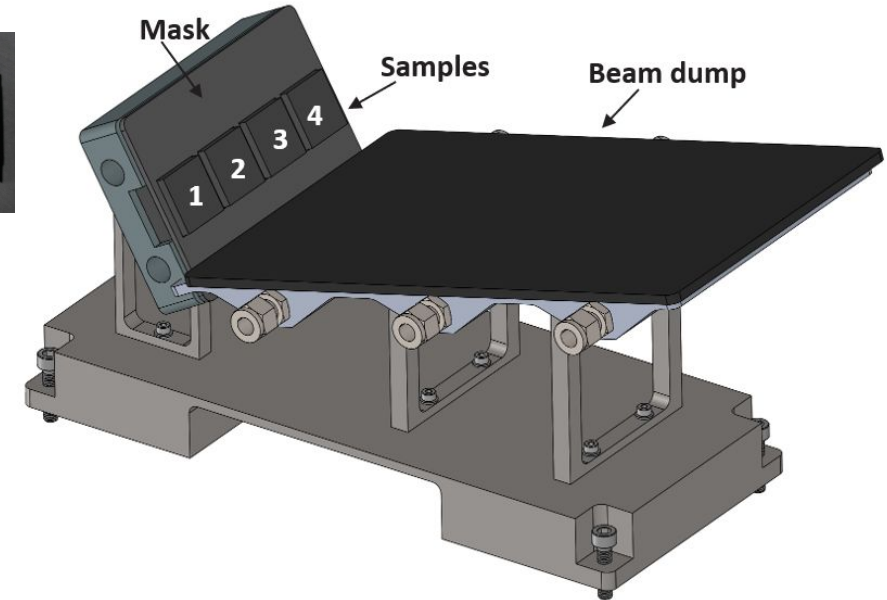
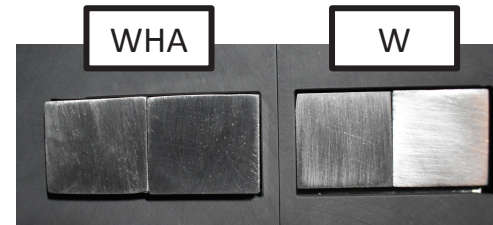
- ARL Sciaky electron beam:
 - 2 A, 17 kV electron beam
 - Focus down to ~ 1 mm scale.
 - Target peak heat fluxes: $100\text{-}500 \text{ MW/m}^2$
 - Target heat flux factors: $40\text{-}100 \text{ MW}\cdot\text{s}^{0.5}/\text{m}^2$
 - PRD high end limit for ELMs, lower limits for disruptions.



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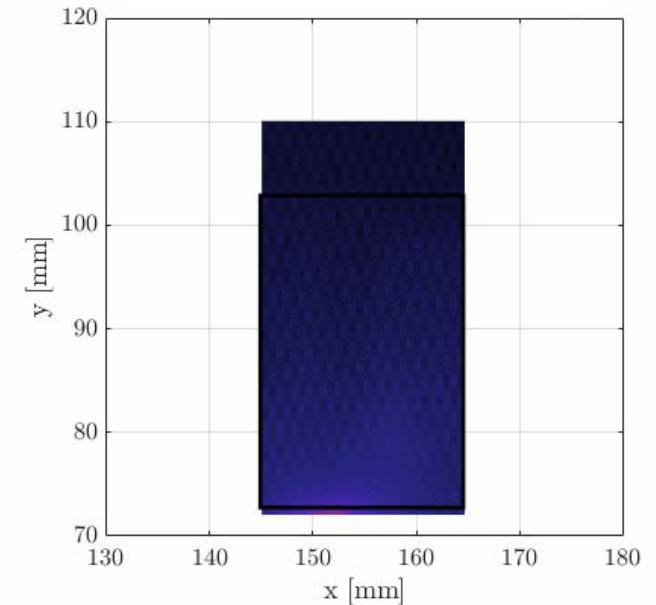
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- side-by-side comparison of WHA (Elmet ET97) and pure W tiles (hot rolled)



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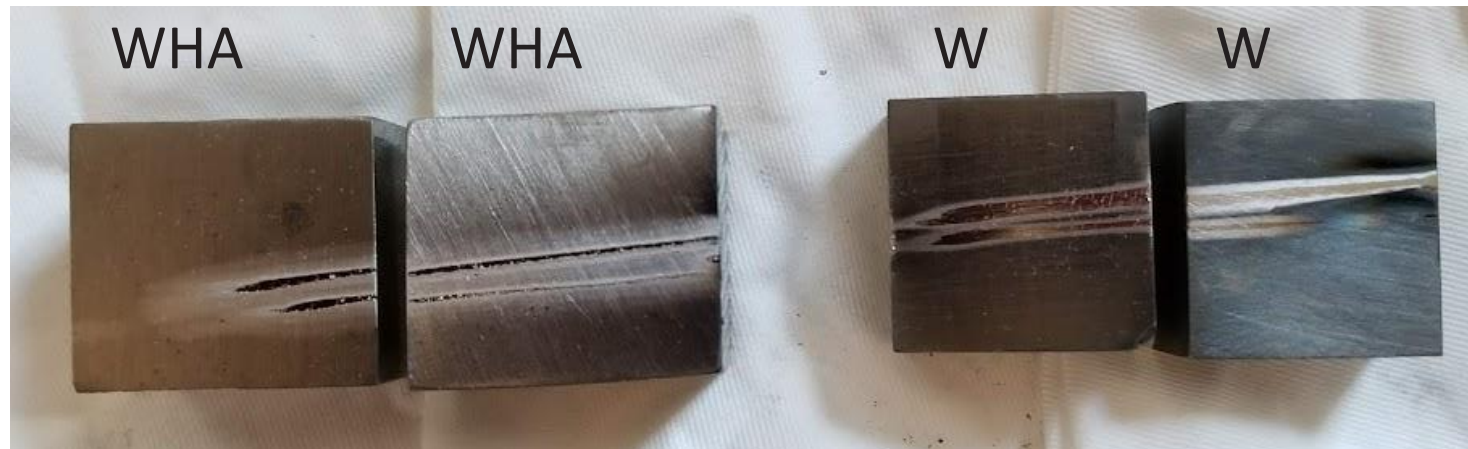


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- side-by-side comparison of WHA (Elmet ET97) and pure W tiles (hot rolled)
- diagnostics: IR and visible cameras, rear TC



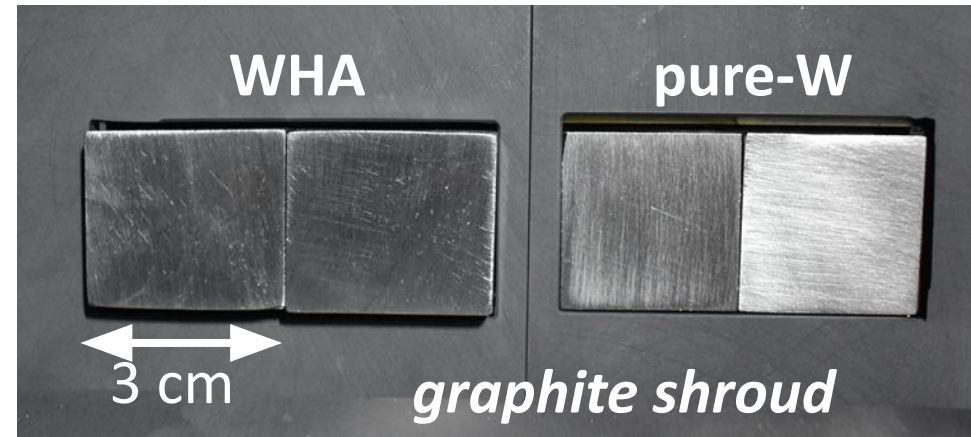
Surface Flash Heating Shows Similar Melt Behavior

- estimated peak heat flux of $\sim 500 \text{ MW/m}^2$ and a beam velocity of 120 mm/s with a FWHM of $\sim 3 \text{ mm}$ using simulation workflow benchmarking energy input via TCs
- suggest that flash melting due to disruptions will not be differentiating.
- consistent with previous work using plasma shock exposures [Laas FED 2020].



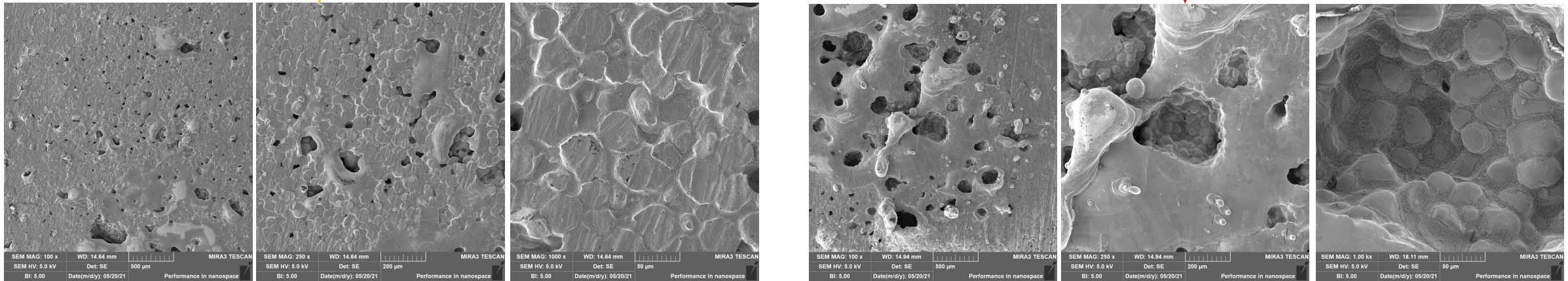
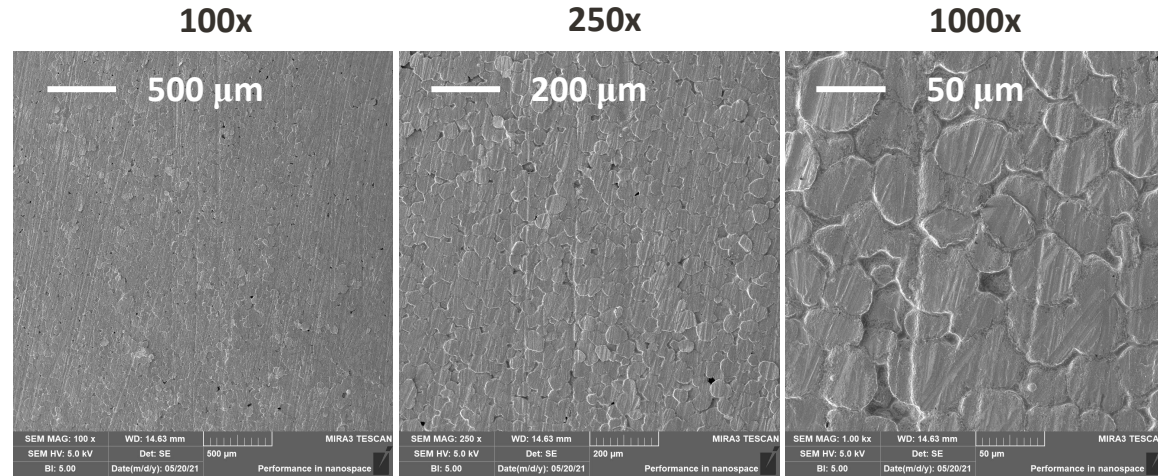
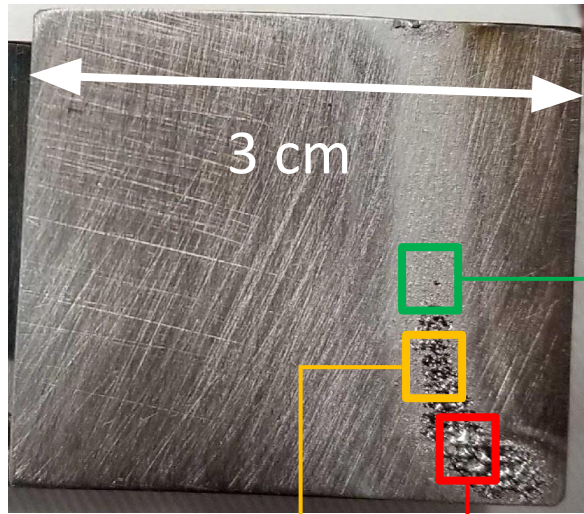
Slower Scans Show Differential Failure Mode

- single(ish) e-beam pass at ~ 50 mm/s
- estimates show WHA has resilience to $\sim 100+$ MW/m² transient loads
- WHA fails at $>70\%$ of the fluxes that melt pure-W
- WHA failure shows mass loss where pure-W does not



challenges w/ beam control and interpretation support FESAC-LRP recommendation for 'additional high heat flux testing facilities'

SEM Analysis Shows Material Responses



e-beam appears to have passed over the bottom of the sample twice leading to some differential melt/material loss behavior on sample

Summary of Results and Next Steps

- SPARC material selection process in early 2021 identified tungsten but allowed for the possibility of tungsten heavy alloy
 - INFUSE project pivoted in scope to compare pure-W and WHA, but maintained original project aim to inform material selection
- differential behavior, shown at slower speed with mass loss and binder migration observed at heat fluxes >70% of those that would melt pure-W
- this work (+ DiMES testing of WHA on DIII-D) helped inform SPARC's decision for partial use of WHA in lower energy input regions of the PFCs
 - off-midplane limiters (where VDE's go) and inboard limiter (used for start-up)
- next steps:
 - fabricate modifications to test stand to allow comparative testing of pure-W samples
 - obtain tungsten samples from different vendors, with different cutting techniques
 - final e-beam testing to be completed in Q1 2022

Impacts on SPARC

- HHF tests provide useful information to guide material selection of SPARC plasma-facing materials
- CFS has access to a high heat flux exposure facility that allows for straightforward comparison (e.g. 'A to B') tests between material samples to inform internal decision making
- CFS and ORNL can now move on to comparative testing of fabrication approaches that help maintain cost and schedule w/o impacting performance
- aim is to have results to inform PDR, scheduled for March 2022

INFUSE Programs on the SPARC Timeline

